

# Robust passification via static output feedback - LMI results

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## Passification and Passivity-based techniques :

- **linear** and nonlinear control
- **simplicity** and physical meaning
- **robustness**
- applications to adaptive control, control of partially linear composite systems, **flight control**, process control...

## Passification of LTI systems :

- SISO and **MIMO**
- SOF for Strict Positive Real  $\Leftrightarrow$  hyper-minimum-phasesness
- Proof of robustness w.r.t. parametric uncertainty (**norm-bounded**)
- Passification of non square systems: **G-passification**

Let an LTI uncertain system:

$$W(s, \Delta) \sim \begin{cases} \dot{x} = A(\Delta)x + Bu \\ y = Cx \end{cases}$$

rational with respect to  $\Delta$

$$A(\Delta) = A + B_{\Delta}\Delta(I - D_{\Delta}\Delta)^{-1}C_{\Delta}$$

uncertain constant real or complex norm-bounded:

$$\Delta^{\mathbb{C}} = \{\Delta \in \mathbb{C}^{m_{\Delta} \times l_{\Delta}} : \Delta^* \Delta \leq I\},$$

$$\Delta^{\mathbb{R}} = \{\Delta \in \mathbb{R}^{m_{\Delta} \times l_{\Delta}} : \Delta^T \Delta \leq I\}.$$

And let  $G \in \mathbb{C}^{m \times p}$  be **given**, where  $B \in \mathbb{C}^{n \times m}$  and  $C \in \mathbb{C}^{p \times n}$

## Robust $G$ -Hyper-Minimum-Phaseness

The system is robustly  $G$ -HMP if  $\forall \Delta \in \Delta$

$$\phi(s, \Delta) = \det(sI - A(\Delta)) \det GW(s, \Delta) = \det \begin{bmatrix} sI - A(\Delta) & -B \\ GC & 0 \end{bmatrix}$$

is Hurwitz and the high-frequency gain of  $GW(s, \Delta)$  is a square symmetric positive definite matrix:  $GC B = B^* C^* G^* > 0$ .

- Generalizes HMP to non-square systems.
- Robustness: infinite number of conditions to test.

## Parameter-dependent and unique static output-feedback

$$\text{PD-SOF : } u = \mathbf{K}(\Delta)y + v \quad \text{SOF : } u = \mathbf{K}y + v$$

## Robust $G$ -Passive control

The closed-loop system is robustly strictly  $G$ -passive if  $\forall \Delta \in \Delta$   
there exists a quadratic PD storage function  $V(x, \Delta) = x^* \mathbf{H}(\Delta)x > 0$   
and a scalar  $\rho(\Delta) > 0$  such that

$$V(x(t), \Delta) \leq V(x(0), \Delta) + \int_0^t \left[ v(\theta)^* G y(\theta) - \rho(\Delta) |x(\theta)|^2 \right] d\theta$$

- Generalizes strict passivity for non-square systems
- $G$ -passification : find  $\mathbf{K}$  that makes the closed-loop  $G$ -passive
- $G$ -passification of  $W(s) \neq$  Passification of  $GW(s)$

Theorem 1 : [Fradkov 1976-2003] Equivalence of

- ①  $W(s, \Delta)$  is robustly  $G$ -HMP
- ②  $W(s, \Delta)$  is robustly  $G$ -passifiable by PD-SOF  $\mathbf{K}(\Delta)$
- ③  $\exists \mathbf{K}$  unique that robustly  $G$ -passificates  $W(s, \Delta)$

Proof (Sketch)

$G$ -HMP  $\Rightarrow$  High gain control for any  $\Delta$ :

$$\mathbf{K}(\Delta) = -\mathbf{k}(\Delta)G \quad : \quad \mathbf{k}(\Delta) > 0 \quad , \quad \text{sufficiently large}$$

Well-posedness of uncertain modeling:  $\mathbf{K} = -\max_{\Delta \in \Delta} \mathbf{k}(\Delta)G$

Outline

- ① LMI results for robust  $G$ -HMP analysis
  - ③ LMI results for robust  $G$ -passifying SOF design
- $\rightarrow$  Numerical example : cruise missile model.

**Theorem 1** *Let the following matrices*

$$N = (GC)^\perp, \quad M = (NN^* + BB^*)^{-1}, \quad \tilde{A} = N^*MAN.$$

$W(s, \Delta)$ ,  $\Delta \in \mathbb{A}^{\mathbb{C}}$  *is robustly  $G$ -HMP*

*if and only if  $GC B > 0$  and  $\exists \mathbf{P} > 0 \in \mathbb{C}$*

$$\begin{bmatrix} \mathbf{P}\tilde{A} + \tilde{A}^*\mathbf{P} & \mathbf{P}N^*MB_\Delta \\ B_\Delta^*MNP & -I \end{bmatrix} + \begin{bmatrix} N^*C_\Delta^* \\ D_\Delta^* \end{bmatrix} \begin{bmatrix} N^*C_\Delta^* \\ D_\Delta^* \end{bmatrix}^* < 0$$

*where  $N = (GC)^\perp$  and  $M = (NN^* + BB^*)^{-1}$ .*

*In case  $\Delta \in \mathbb{A}^{\mathbb{R}}$ ,  $\mathbf{P} \in \mathbb{R}$ ; LMI conditions are only sufficient.*

**Proof**

Robust  $G$ -HMP is reformulated as

the robust Hurwitz stability of a reduced order system.

**Theorem 2**  $W(s, \Delta)$  is uniformly robustly strictly  $G$ -passifiable via SOF if and only if  $\exists \mathbf{H} > 0 \in \mathbb{C}, \exists \mathbf{K} \in \mathbb{C}$ :

$$\mathbf{H}B = C^*G^*$$

$$\begin{bmatrix} \mathbf{H}A + A^*\mathbf{H} + C^*(G^*\mathbf{K} + \mathbf{K}^*G)C & \mathbf{H}B_\Delta \\ B_\Delta^*\mathbf{H} & -I \end{bmatrix} + \begin{bmatrix} C_\Delta^* \\ D_\Delta^* \end{bmatrix} \begin{bmatrix} C_\Delta^* \\ D_\Delta^* \end{bmatrix}^* < 0$$

**Proof**

Classical LMI results for 'quadratic' stability

→ Uniform storage function  $V(x, \Delta) = V(x) = x^*\mathbf{H}x$ .



**Theorem 3**  $W(s, \Delta)$  is uniformly robustly strictly  $G$ -passifiable via SOF if and only if  $\exists \mathbf{H} > 0 \in \mathbb{C}, \exists \mathbf{K} \in \mathbb{C}$ :

$$\mathbf{H}B = C^*G^*$$

$$\begin{bmatrix} \mathbf{H}A + A^*\mathbf{H} + C^*(G^*\mathbf{K} + \mathbf{K}^*G)C & \mathbf{H}B_\Delta \\ B_\Delta^*\mathbf{H} & -I \end{bmatrix} + \begin{bmatrix} C_\Delta^* \\ D_\Delta^* \end{bmatrix} \begin{bmatrix} C_\Delta^* \\ D_\Delta^* \end{bmatrix}^* < 0$$

## Remarks

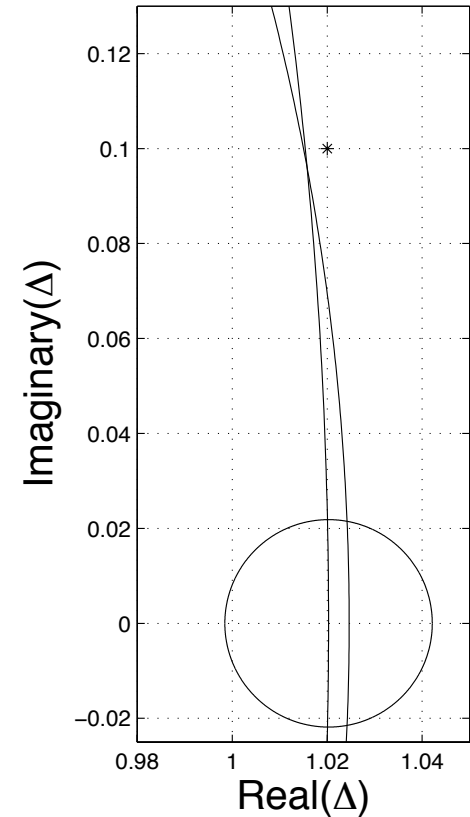
- ★ Thm 2  $\Rightarrow$  Thm 1 with  $\mathbf{P} = N^*\mathbf{H}N$  (conjecture : converse also holds)
- ★ PB : design  $\mathbf{K}$  and  $G$  simultaneously ?  
LMI problem if  $\exists \mathbf{S}$  such that  $\mathbf{P}B = B\mathbf{S}$  (conservative)
- ★ Always possible to take  $\mathbf{K} = -\mathbf{k}G$  if feasible.
- ★ Possible to add LMI constraints on  $\mathbf{K}$ , e.g. find  $\mathbf{K}$  with minimum norm.

## Model definition

- 4th order model of lateral dynamics for cruise missile + actuator dynamics
- Dynamics depend on altitude  $h \in [\underline{h} \ \bar{h}] \subset \mathbb{R}^+$  (converted into  $\Delta \in \Delta^R$ )
- Measured outputs:  
yaw angle  $\varphi(t)$ , yaw angular rate  $r(t)$  and the rudder deflection angle  $\delta_r(t)$
- Control input: rudder servo command signal
- $G$  is chosen *a priori* such that  $GCB > 0$ .

## Robust $G$ -HMP analysis

- ★ For  $\underline{h} = 0$  and  $\bar{h} = 10\text{km}$  : **feasible**
- ★ For  $\underline{h} = 9.9925\text{km}$  and  $\bar{h} = 10.2105\text{km}$  : **feasible**
- ★ For  $\underline{h} = 0$  and  $\bar{h} = 10.2105\text{km}$  : **infeasible**
  - $h = 10.1 + 0.5i$  makes system non  $G$ -HMP.
  - Conservatism for real-valued uncertainty.



→ Exists a SOF for  $h \in [0 \ 10.2105]$ , cannot be found with Thm 2.

# Numerical example : cruise missile

Robust  $G$ -passifying SOF design Assume  $h \in [0 \ 10]$

★ Thm 2

$$\rightarrow \mathbf{K}_1 = - \begin{bmatrix} 79.28 & 50.34 & 11.92 \end{bmatrix}$$

★ Thm 2,  $\min \|\mathbf{K}\|$ :

$$\rightarrow \mathbf{K}_2 = - \begin{bmatrix} 60.75 & 34.47 & 10.67 \end{bmatrix}$$

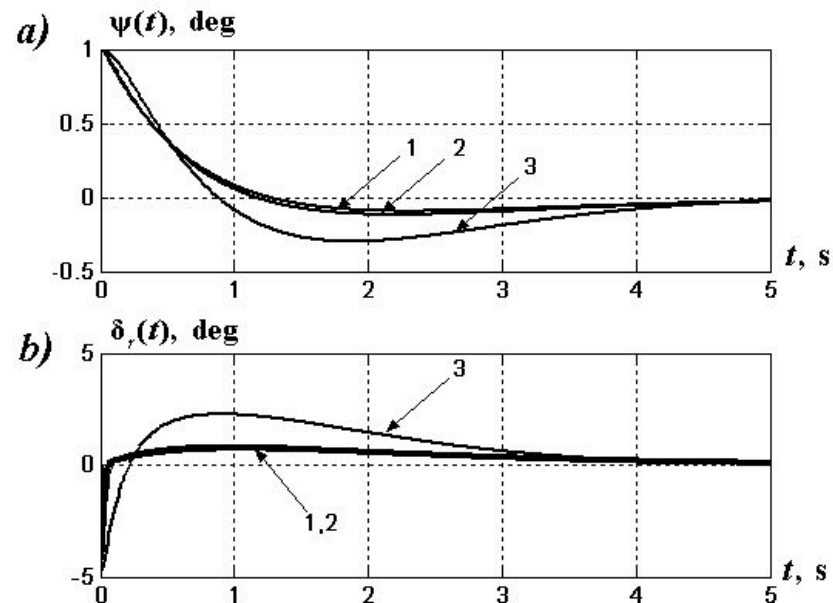
★ Thm 2,  $\min_{\mathbf{K}=-\mathbf{k}_G \mathbf{k}, :}$

$$\rightarrow \mathbf{K}_3 = - \begin{bmatrix} 118.53 & 44.45 & 14.82 \end{bmatrix}$$

Yaw angle and rudder deflection

for control  $\mathbf{K}_2$

and for  $h = 0.1, 5, 9$



- Non-conservative (complex case) LMI conditions of robust strict  $G$ -passification
- Conservative LMI design method
  
- ★ Design simultaneously  $\mathbf{K}$  and  $G$
- ★ Design of robust  $G$ -passifying adaptive control  $u(t) = \mathbf{K}(t)y(t)$