

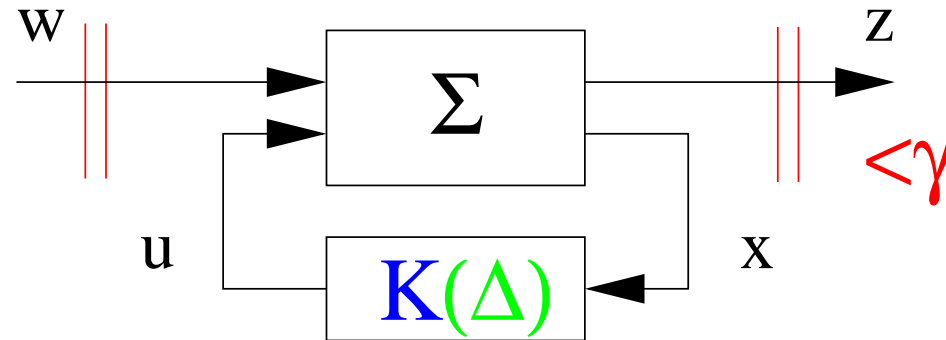
# LMI Results for Resilient State-Feedback with $H_\infty$ Performance

Dimitri PEAUCELLE & Denis ARZELIER & Christophe FARGES

LAAS-CNRS

Toulouse, FRANCE

Considered problem: Resilient state-feedback design with  $H_\infty$  performance.



Fragile: Uncertainties on the control destroy expected closed-loop properties.

Uncertainties on the control:

- Tuning margins for practical implementation
- Implementation errors
- Finite-precision elements and computation.

Resilient: Not fragile

State-space LTI systems in continuous-time with performance output/input signals:

$$\Sigma \sim \begin{pmatrix} \dot{x} \\ z \\ y \end{pmatrix} = \begin{bmatrix} A & B_w & B \\ C_z & D_{zw} & D_{zu} \\ C & D_{yw} & D \end{bmatrix} \begin{pmatrix} x \\ w \\ u \end{pmatrix}$$

Alternative representation:

$$Q_x \begin{pmatrix} x \\ -\dot{x} \end{pmatrix} + Q_w \begin{pmatrix} w \\ -z \end{pmatrix} + Q_u \begin{pmatrix} u \\ -y \end{pmatrix} = 0 \quad , \quad Q_x = \begin{bmatrix} A & I \\ C_z & 0 \\ C_y & 0 \end{bmatrix} \quad \dots$$

Define  $\Sigma \star \mathbf{K}$  the closed-loop system with  $u = \mathbf{K}y$ .

Derived from results published at IFAC'02 Barcelona, ECC'03 Cambridge:

**Theorem 1** *There exists a solution to the following matrix inequality problem*

$$Q_x \begin{bmatrix} 0 & \mathbf{P} \\ \mathbf{P} & 0 \end{bmatrix} Q_x^T < Q_w \begin{bmatrix} -1 & 0 \\ 0 & \gamma^2 \mathbf{I} \end{bmatrix} Q_w^T + Q_u \begin{bmatrix} \mathbf{X} & \mathbf{Y} \\ \mathbf{Y}^T & \mathbf{Z} \end{bmatrix} Q_u^T$$
$$\mathbf{P} > 0 \quad , \quad \mathbf{Z} > 0 \quad , \quad \mathbf{X} \leq \mathbf{Y}\mathbf{Z}^{-1}\mathbf{Y}^T$$

if and only if all controls  $u = \mathbf{K}y$  that satisfy the quadratic constraint

$$\mathbf{X} + \mathbf{K}\mathbf{Y}^T + \mathbf{Y}\mathbf{K}^T + \mathbf{K}\mathbf{Z}\mathbf{K}^T \leq 0$$

perform the closed-loop  $H_\infty$  performance  $\|\Sigma \star \mathbf{K}\|_\infty \leq \gamma$

Remarks:

- Non-linear matrix inequalities, NP-hard in general
- Design of sets of controllers (matrix  $\{\mathbf{X}, \mathbf{Y}, \mathbf{Z}\}$ —ellipsoids)

**Theorem 2** *Let the following matrices*

$$\hat{Q}_x = \begin{bmatrix} A & I \\ C_z & 0 \end{bmatrix}, \quad \hat{Q}_w = \begin{bmatrix} B_w & 0 \\ D_{zw} & I \end{bmatrix}, \quad \hat{Q}_u = \begin{bmatrix} B & I \\ D_{zu} & 0 \end{bmatrix}$$

*There exists a solution to the following LMI problem*

$$\hat{Q}_x \begin{bmatrix} 0 & \mathbf{P} \\ \mathbf{P} & 0 \end{bmatrix} \hat{Q}_x^T < \hat{Q}_w \begin{bmatrix} -I & 0 \\ 0 & \gamma^2 I \end{bmatrix} \hat{Q}_w^T + \hat{Q}_u \begin{bmatrix} \hat{\mathbf{X}} & \hat{\mathbf{Y}} \\ \hat{\mathbf{Y}}^T & -\hat{\mathbf{Z}} \end{bmatrix} \hat{Q}_u^T$$

$$\mathbf{P} > 0, \quad \hat{\mathbf{Z}} > 0, \quad \hat{\mathbf{X}} \leq 0$$

*if and only if all state-feedback gains  $u = \mathbf{K}x$  of the  $\{\mathbf{X}, \mathbf{Y}, \mathbf{Z}\}$ -ellipsoid where*

$$\mathbf{X} = \hat{\mathbf{X}} + \hat{\mathbf{Y}}\hat{\mathbf{Z}}^{-1}\hat{\mathbf{Y}}^T, \quad \mathbf{Y} = \hat{\mathbf{Y}}\hat{\mathbf{Z}}^{-1}\mathbf{P}, \quad \mathbf{Z} = \mathbf{P}\hat{\mathbf{Z}}\mathbf{P}$$

*perform the closed-loop  $H_\infty$  performance  $\|\Sigma \star \mathbf{K}\|_\infty \leq \gamma$*

Remarks:

→ Finding ellipsoidal set of state-feedback controllers is purely LMI.

→  $\mathbf{K}_o = -\mathbf{Y}\mathbf{Z}^{-1} = -\hat{\mathbf{Y}}\mathbf{P}^{-1}$  is the center of the ellipsoidal set.

→ The classical LMI for the design of a unique control gain is a sub-case where

$$\hat{\mathbf{X}} = \mathbf{0} \quad , \quad \mathbf{K} = \mathbf{K}_o$$

and  $\hat{\mathbf{Z}}$  is removed because redundant in the constraints.

Can the LMI design of ellipsoidal sets solve the resilience problem?

→ Avoid sets close to singletons.

→ Specify the set geometry for additive or multiplicative uncertainty on  $\mathbf{K}$ .

→ Find a set that includes a known feedback gain  $K_n$ .

## Corollary 1

If the solution to theorem 2 satisfies simultaneously the LMI constraints

$$\begin{bmatrix} \tau_a \mathbf{I} & \mathbf{P} \\ \mathbf{P} & \hat{\mathbf{Z}} \end{bmatrix} \geq \mathbf{0} \quad , \quad \hat{\mathbf{X}} \leq -\tau_a \delta_a^2 \mathbf{I}$$

then  $\|\Sigma \star K(\Delta)\|_\infty \leq \gamma$  for any additive norm-bounded uncertainty on  $\mathbf{K}_o$  such that:

$$K(\Delta) = \mathbf{K}_o + \Delta \quad : \quad \Delta \Delta^T \leq \delta_a^2 \mathbf{I}$$

Remarks:

- Generate ellipsoidal sets that contain a "sphere" of radius  $\delta_a$ .
- If  $\delta_a = 1/2$  it implies that the gain build out of the rounded coefficients of  $\mathbf{K}_o$  still guarantees the closed-loop stability and  $H_\infty$  performance.

## Corollary 2

If the solution to theorem 2 satisfies simultaneously the LMI constraints

$$\begin{bmatrix} \tau_m \mathbf{I} & S_2 \hat{\mathbf{Y}} \\ \hat{\mathbf{Y}}^T S_2^T & \hat{\mathbf{Z}} \end{bmatrix} \geq \mathbf{0} \quad , \quad \hat{\mathbf{X}} \leq -\tau_m \delta_m^2 S_1 S_1^T$$

then  $\|\Sigma \star K(\Delta)\|_\infty \leq \gamma$  for any multiplicative norm-bounded uncertainty on  $\mathbf{K}_o$  such that:

$$K(\Delta) = (\mathbf{I} + S_1 \Delta S_2) \mathbf{K}_o \quad : \quad \Delta \Delta^T \leq \delta_m^2 \mathbf{I}$$

Remarks:

→ In this case the uncertainty is not totally known *a priori* but related to the designed value  $\mathbf{K}_o$ .

→ Uncertainty is known to have influence only on some elements of  $\mathbf{K}_o$ .

→ Modeling found in [Yee *et al.*, IJSS 2001]

## Corollary 3

*If the solution to theorem 2 satisfies simultaneously the LMI constraints*

$$\begin{bmatrix} \hat{\mathbf{X}} & \bar{\delta} \hat{\mathbf{Y}} \\ \bar{\delta} \hat{\mathbf{Y}}^T & -\hat{\mathbf{Z}} \end{bmatrix} \leq 0$$

*then  $\|\Sigma \star K(\Delta)\|_\infty \leq \gamma$  for any scalar multiplicative uncertainty on  $\mathbf{K}_o$  such that:*

$$K(\Delta) = (1 + \delta)\mathbf{K}_o \quad : \quad |\delta| \leq \bar{\delta}$$

Remarks:

- Allows a set of proportional state-feedback gains.
- $\delta$  is a design parameter for fine tuning.
- Modeling found in [Corrado and Haddad, ACC 1999]

## Example 1: purely academic to illustrate ellipsoids

---

$$A = \begin{bmatrix} 1 & 1 \\ -10 & 1 \end{bmatrix}, \quad B_w = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \quad B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad \gamma = 1$$
$$C_z = \begin{bmatrix} 1 & 1 \end{bmatrix}, \quad D_{zw} = 0.5, \quad D_{zu} = 0.1$$

→ Classical design (single state-feedback):

$$K_1 = \begin{bmatrix} -10.2357 & 12.2276 \end{bmatrix} : \|\Sigma \star K_1\|_\infty = 0.8307$$

Fragile to  $\bar{\delta} = 0.5$  and  $\delta_a = 10$ :

$$\|\Sigma \star (1 - 0.5)K_1\|_\infty = 1.1160, \quad \|\Sigma \star \begin{bmatrix} -2 & 12 \end{bmatrix}\|_\infty = \infty$$

→ New ellipsoidal set design without constraints on the set. Center:

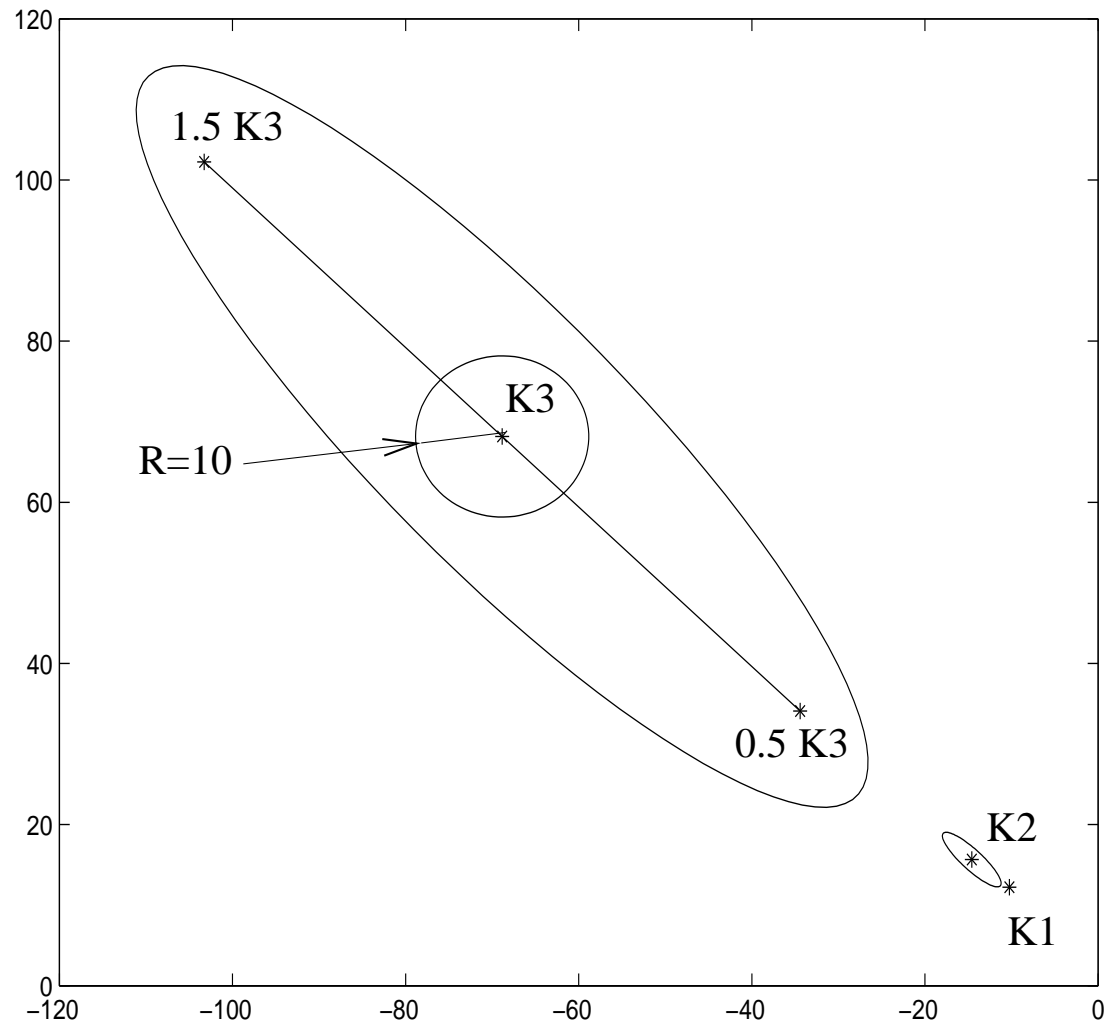
$$K_2 = \begin{bmatrix} -14.5908 & 15.6533 \end{bmatrix} : \|\Sigma \star K_2\|_\infty = 0.7555$$

the obtained set has a volume of 5.62 times the unit circle.

# Example 1: purely academic to illustrate ellipsoids

→ Ellipsoidal set constrained by  $\bar{\delta} = 0.5$  and  $\delta_a = 10$  gives a center:

$$K_3 = \begin{bmatrix} -68.8418 & 68.1654 \end{bmatrix}$$
$$\|\Sigma \star K_3\|_\infty = 0.6977$$



# Conclusion

---

- LMI results for  $H_\infty$  state-feedback design can be extended to resilient design.
- Remains an LMI problem, few additional variables.
- Same procedure can be applied for other state-feedback problems (pole location,  $H_2$ , ...)
- Prospective: extend to full-order dynamic output-feedback.